Le/pets

DESCRIPTION

REINFORCING NON-WOVEN BASE FABRIC

5   Technical Field

    The present invention relates to a reinforcing non-woven base fabric that is used for externally reinforcing and repairing a concrete structure, and also concerns a reinforcing non-woven base fabric used for FRP.

10

Background Art

    In order to reinforce and repair FRP or a concrete structure, a so-called high-strength fiber sheet having a specific gravity smaller than metal and strength higher
15   than metal is inserted or bonded thereto.

    The high-strength fibers are allowed to further increase the strength thereof when a number of fibers are arranged in a direction in which greater strength is required. However, the high-strength fibers in a yarn
20   state cause difficulty in handling and time-consuming tasks in aligning yarns one by one; therefore, the high-strength fibers in a sheet state are used in most cases.

    With respect to the high-strength fiber sheet, a sheet made by forming glass fibers into a sheet shape has been
25   known (for example, see Japanese Patent Application Laid-

Open No. 8-142238, Fig. 2, and Japanese Patent Application
Laid-Open No. 2001-159047).

In the case when glass fibers are formed into a sheet
shape, a material prepared by impregnating glass fibers
5   with a bonding-agent solution is generally used, and high-
strength fibers, for example, carbon fiber yarns, are
bonded to the material to maintain the sheet shape. The
glass fiber yarn is composed of not a single fiber, but a
bunch of glass fibers, with the result that voids tend to
10   exist between fibers. Even when the bunch of glass fibers
is impregnated with the bonding-agent solution, these voids
are not filled with the solution. Depending on the bonding
agents, during drying and bonding processes after the
impregnation, voids tend to generate inside the fiber yarns.
15   Consequently, a reinforcing non-woven base fabric including
a number of voids therein is used for reinforcing FRP or a
concrete structure, with the result that the strength of
the reinforced FRP or the reinforced concrete is lowered.
A bonding agent, such as an acrylic resin, a nylon resin
20   and polyester, to be normally used for bonding the high-
strength fibers and the shape-retaining fibers to each
other tends to absorb moisture during production and
storage, with the result that the adhesive property to the
matrix of the FRP or the concrete is lowered to cause a
25   reduction in the reinforcing performance. The moisture is

evaporated to expand to sometimes cause a deformation in the matrix resin and damages thereto. The glass fibers that have been often used conventionally has a high specific gravity, that is, in a level of 2.5, to cause an increase in the weight per unit area as a whole and insufficient flexibility; consequently, the conventional glass fibers cause a difficulty in handling due to an insufficient following property to curved faces and the like.

Disclosure of Invention

(Technical subjects to be solved by the present invention)

The present invention has been made to solve the above-mentioned problems, and its objective is to provide a reinforcing non-woven base fabric that is free from adverse effects such as moisture-absorbing property and voids, and capable of exerting superior properties such as flexibility and light weight.

(Means to solve problems)

The present invention relates to a reinforcing non-woven base fabric that is made by forming reinforcing fiber yarns into a sheet shape using a support fibrous member, and in the reinforcing non-woven base fabric, the support fibrous member is made of multifilament yarns using

composite fibers constituted by at least two or more polymers having a difference in melting points.

Brief Description of Drawings

5   Fig. 1 is a schematic structural drawing that shows a fusion-bonding mesh manufacturing machine;

     Fig. 2 is a schematic structural drawing that shows a reinforcing non-woven base fabric manufacturing machine of the present invention;

10   Fig. 3 is a schematic structural drawing that shows a glass mesh manufacturing machine;

     Fig. 4 is an electron microscopic photograph that shows a fiber form in a cross-section of a reinforcing non-woven base fabric obtained in example 1;

15   Fig. 5 is a schematic structural drawing that shows a reinforcing non-woven base fabric manufacturing machine;

     Fig. 6 is an electron microscopic photograph that shows a fiber form in a cross-section of a reinforcing non-woven base fabric obtained in comparative example 1;

20   Fig. 7 is a schematic cross-sectional view of a monofilament used for a support fibrous member;

     Fig. 8 is a schematic cross-sectional view of a reinforcing non-woven base fabric in accordance with the present invention.

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Best Mode for Carrying Out the Invention

Reinforcing fiber yarns forming a sheet-shaped member of the present invention include carbon fibers, glass fibers, boron fibers, steel fibers, aramid fibers, vinylon

5   fibers and the like, and are made of multifilaments that form a flat shape without twists. The multifilaments are preferably designed to have a degree of flatness of not less than 2, more preferably not less than 10; here, the degree of flatness is defined as a ratio of the width to

10   the thickness. Particularly preferable degree of flatness is in a range from 20 to 700. Here, the multifilaments having a degree of flatness in a range from 20 to 700 are obtained by further subjecting multifilaments that have a flat shape without twists to a fiber-opening process.

15   The fiber-opening process refers to a process in which a bunch of fibers, which is an aggregate of a plurality of filaments, are separated in the fiber width direction, and the fiber-opening process is applied to the bunch of fibers so that the width of the bunch of fibers is further widened.

20   Those yarns obtained through the fiber-opening process are referred to as fiber extended yarns. In the present invention, with respect to the multifilaments or laminated multifilaments, those having a width that is widened 2 to 5 times, preferably 2 to 4 times, the width of the original

25   multifilaments through the fiber-opening process may be

used. For example, a carbon-fiber multifilament having a

width of about 6 mm, formed by combining 12,000 carbon

fibers having a diameter of 7 μm with one another, is

subjected to a fiber-opening process to form a flat

5   multifilament (fiber extended yarn) having a width of 20 mm.

With respect to the support fibrous member to be used

in the present invention, composite fibers, constituted by

at least two or more polymers having a difference in

melting points, are used. The composite fiber means the

10   one in which an arrangement of respective components in a

cross section is shown in various morphology, such as

parallel, core-sheath , grains, radiation, mosaic, sea

islands and nebula. From the viewpoint of productivity,

shape-retaining property and fusion-bonding property, a

15   two-layered product with two components having a core-

sheath structure is preferably used. Preferably, composite

fibers having a core-sheath structure in which the sheath

portion is formed by a polymer having a lower melting point

than that of the core portion are used. From the viewpoint

20   of productivity, the difference in melting points is

preferably not less than 20°C, more preferably not less

than 30°C. In the case of the application of fibers made

of a single component, the fibers might be cut in a fusion-

bonding process; however, the application of fibers using

25   polymers having a difference in melting points makes it

possible to prevent the support fibrous member from being cut or deformed when the reinforcing fiber yarns and the support fibrous member are thermally fusion-bonded at a melting temperature on the low melting point side. The

5   support fiber member is flattened by thermo-compression processes, and the degree of irregularities in the thickness direction is consequently lowered, resulting in excellence in flatness.

The support fibrous member to be used in the present

10   invention is constituted by multifilament yarns using composite fibers. The application of monofilament is not desirable because the monofilament lacks in flexibility. In the case when multifilaments consisting of a single fiber are used, it becomes very difficult to remove voids

15   derived from gaps between the single fibers as described earlier; consequently, the application of the multifilaments of this type is not desirable due to a reduction in strength due to voids. In the present invention, multifilaments, having 30 or more filaments, are

20   preferably used. The thickness of filaments is preferably in a range from 100 d to 1000 d.

With respect to the material for the multifilament yarns, both of a low melting point polymer and a high melting point polymer are preferably olefin-based to form

25   multifilaments. . The olefin has a very low specific

gravity in comparison with other thermoplastic resins and

inorganic fibers. The olefin has a specific gravity of

0.90 to 0.98; in contrast, generally-used polymer materials

have a specific gravity of about 1.5 and inorganic fibers

5   have a specific gravity of about 1.8 to 2.7, which is

comparatively heavy. The olefin has a hydrophobic property,

and has no moisture-absorbing property. Even if any

absorbed moisture is present between filaments, the amount

thereof is very small, and the moisture evaporates during a

10 fusion-bonding process. More preferably, a combination of

a polypropylene polymer serving as the high melting point

polymer and polyethylene or low melting point polypropylene

serving as a low melting point polymer, that is, a

combination of polyolefin polymers in a narrow sense, may

15 be used. More specifically, preferable examples of the

structure and material include: a core-sheath structure

having a polypropylene (core portion)/polyethylene (sheath

portion) combination, or a polypropylene (core portion)/low

melting point polypropylene (sheath portion) combination.

20   Polyolefin-based multifilaments to be used for the

support fibrous member of the present invention have no

bonding property to high-strength fibers, such as carbon

fibers, glass fibers, boron fibers, steel fibers, aramid

fibers and vinylon fibers. In the case of conventional

25 support materials for glass fibers, any low melting point

binder, such as nylon and polyester, is adhered thereto so that the high-strength fibers and the support fibrous member are bonded to each other; however, in the present invention, no additional binder is required. In other

5 words, the olefin-based polymer of a low-melting portion in composite fibers is anchored onto the high-strength fibers through the fusion-bonding; thus, a sheet shape is retained through a so-called anchor effect. One of the features of the present invention lies in the finding that a sheet-

10 retaining is possible through the anchoring effect, even when low melting point olefin-based multifilaments, which inherently have no adhesive property, are used.

The support fiber material to be used in the present invention allows reinforced fiber yarns to be formed into a

15 sheet shape by using a structure that is different from a fabric, that is, a non-woven fabric structure, and, for example, a method using the support fiber material as wefts and the like and a method using the support fiber material as a mesh structure are proposed.

20 The mesh structure can be manufactured through the following processes: multifilament yarns made of composite fibers, aligned in a length direction, and multifilament yarns made of composite fibers, aligned in a width direction, are alternately laminated to form two layers and

25 more so as to form an integral sheet shape, and the

laminated body is thermo-compressed by applying a temperature lower than the melting temperature of the high melting point polymer thereto. These thermo-compression processes allow the heat bonding resin in low melting point

5   portions in the composite fibers to fuse, making it possible to provide a mesh structure having a stable shape that is free from voids. The mesh structure is formed by alternately laminating two or more layers; therefore, different from a textile or knit structure, the warp is

10 less susceptible to bending, that is, no stress concentration is imposed on the warp. In the present invention, it is not necessarily required for multifilament yarns of composite fibers to be used in both of the length direction and width direction; however, from the viewpoints

15 of a reduced thickness and a stable mesh structure, multifilament yarns of composite fibers are preferably used in both of the two directions.

In the present invention, the reinforcing fiber yarns are retained into a sheet shape by the support fibrous

20 member so that a reinforcing non-woven base fabric is formed.

The shape-retained sheet may be a uniaxial reinforcing fiber sheet in which a plurality of reinforcing fiber yarns are aligned in one direction. Alternatively, the shape-

25 retained sheet may be a biaxial reinforcing fiber sheet in

which a warp sheet composed of reinforcing fiber yarns that are aligned in a length direction and a weft sheet composed of reinforcing fiber yarns that are aligned in a width direction are laminated. The shape-retained sheet may be a multi-axial reinforcing fiber yarn sheet that is formed by laminating a yarn sheet made of reinforcing fiber yarns which, supposing that the length direction of the sheet is $0°$, are aligned in $0°$-direction, a yarn sheet made of reinforcing fiber yarns which are aligned in a $+\alpha°$ -direction as well as in a $-\alpha°$ -direction ($0 < \alpha < 90$) and a yarn sheet made of reinforcing fiber yarns which are aligned in a $0°$-direction and/or in a $90°$-direction. With respect to the mode in which the reinforcing fiber yarns are aligned, they may be aligned with fixed intervals or may be aligned closely.

In the case when the retained shape forms the uniaxial reinforcing fiber sheet, a so-called shape-retaining method only by the weft, which places a plurality of support fibrous members side by side in a direction virtually perpendicular to the direction (hereinafter, referred to as "reinforcing fiber yarn direction") in which the fiber yarns are aligned so that the support fibrous members and the sheet-shaped member are shape-retained through a fusion-bonding process, may be used. In addition to the support fibrous members aligned in the virtually

perpendicular direction, a plurality of support fibrous

members may be placed side by side virtually in parallel

with the reinforcing fiber yarn direction so that the

support fibrous members in a mesh state may be fusion-

5   bonded with the sheet-shaped member and shape-retained. In

the case when the shape-retaining process is carried out

with the support fibrous members being maintained in the

mesh state, after the support fibrous members have been

preliminarily formed into a desired mesh state through a

10   fusion-bonding process or the like, the resulting mesh-

state member may be superposed on the sheet-shaped member

and thermally bonded with each other.

When the reinforcing fiber yarns are shape-retained

into a uniaxial reinforcing fiber yarn sheet, a structure

15   in which at least two or more layers of reinforcing fiber

yarns (for example, the group of warp yarns) and support

fibrous members (for example, the group of weft yarns) are

laminated with each other is preferably used so that

contact points (lines) between the group of warp yarns and

20   the group of weft yarns are fusion-bonded so as to carry

out a shape-retaining process. More preferably, as shown

in Fig. 8, two upper and lower layers 82 and 83 constituted

by groups of warp yarns with a fixed interval are prepared,

with an intermediate layer 81 constituted by a group of

25   weft yarns made of support fibrous members being

interpolated therebetween to prepare a three-layered
structure; thus, a laminated structure in which the lower
layer is placed with a 1/2-pitch offset so that each yarn
of the lower-layer yarn group is positioned between the

5 yarns of the upper-layer yarn group is preferably used.

In the case when the retained shape forms the biaxial
reinforcing fiber sheet, a sheet in which reinforcing fiber
yarns are preliminarily formed in a biaxial format is used
and groups of support fibrous member yarns (a plurality of

10 yarns aligned in parallel with one another or in a mesh
pattern) may be fusion-bonded and shape-retained on the
upper face, intermediate face and/or lower face of the
sheet. Simultaneously as the biaxial reinforcing fiber
yarns are formed, the support fibrous members may be

15 inserted and fusion-bonded and shape-retained. In this
case, the shaping process is preferably carried out so that
at least the direction of the support fibrous members and
the direction of the reinforcing fiber yarns are allowed to
make virtually 90 degrees. Moreover, the uniaxial

20 reinforcing fiber sheet reinforcing non-woven base fabrics,
obtained as described above, may be laminated with one
another, with the direction of the reinforcing fiber yarns
being offset by about 90 degrees, so that these may be
again fusion-bonded to obtain a reinforcing non-woven base

25 fabric. Moreover, the uniaxial reinforcing fiber sheet

reinforcing non-woven base fabrics prior to the fusion-bonding process may be laminated with one another, with the direction of the reinforcing fiber yarns being offset by about 90 degrees, and fusion-bonded.

5   In the case when the retained shape forms the multi-axial reinforcing fiber sheet, instead of the structure of the biaxial reinforce fiber sheet in which uniaxial reinforcing fiber sheet reinforcing non-woven base fabrics are laminated with a 90-degree offset, a plurality of the

10   base fabrics may be laminated with an offset of $\alpha°$-degrees ($0 < \alpha < 90$) so that a multi-axial reinforcing fiber sheet reinforcing non-woven base fabric is obtained in the same manner as the biaxial reinforcing fiber sheet reinforcing non-woven base fabric. The size of α may be appropriately

15   selected depending on the number of desired laminated layers.

The fusion-bonding process is carried out while the laminated body of the reinforcing fiber yarns and the support fibrous members is heated and pressurized.

20   The number of the support fibrous members to be used and the gap between the parallel alignments are not particularly limited as far as the sheet-shaped member is shape-retained, and may be appropriately selected depending on the purpose for the reinforcing non-woven base fabric,

25   the size and the method thereof, as well as on the kind,

the width and the manufacturing method of the fiber

extended yarns.

The following description will discuss a method for

continuously manufacturing a reinforcing non-woven fabric

5   of the present invention, and a machine used for

manufacturing such a fabric.

(1) A manufacturing method and a manufacturing machine for

a reinforcing non-woven base fabric formed of uniaxial

reinforcing fibers.

10   (i) A reinforcing non-woven base fabric manufacturing

machine, which is constituted by at least: a device that

continuously supplies a pair of selvage yarns on both of

the right and left sides; a device that continuously

supplies a weft of multifilament heat-bonding yarn made of

15   composite fibers so that the weft is passed over the paired

selvage yarns in a winding manner so as to proceed; a

device that continuously supplies a number of warps of

reinforcing fiber yarns onto the upper face and lower face

of the winding weft to carry out warping and matching

20   processes; and a device which, after the warp and the wefts

have been laminated, carries out heating and pressurizing

processes to fuse the low-melting portions of the weft so

that the warp and the wefts are bonded to each other

through the fusion-bonding process, and takes up the joined

25   non-woven base fabric; and a manufacturing method by which

the manufacturing machine is operated.

(ii) A reinforcing non-woven base fabric manufacturing machine, which is constituted by at least: a device that continuously supplies a number of warps so as to carry out

5 warping and matching processes; a device that feeds a mesh-shaped sheet formed by multifilament heat bonding yarns made of composite fibers; and a device which, immediately after the warps have been subjected to the warping process and supplied, inserts the mesh-shaped sheet formed by

10 multifilament heat bonding yarns made of composite fibers from the upper portion or the lower portion, or from both of the upper and lower portions, so as to fuse the mesh-shaped sheet by heating and pressurizing so that the mesh-shaped sheet formed by multifilament fusion-bonding yarns

15 made of composite fibers is bonded to a non-woven base fabric through the heat bonding with the warps, and takes up the resulting joined non-woven base fabric; and a manufacturing method by which the manufacturing machine is operated.

20 (iii) A reinforcing non-woven base fabric manufacturing machine, which is constituted by at least: a device that continuously supplies a pair of selvage yarns on both of the right and left sides; a device that continuously supplies a weft of multifilament fusion-

25 bonding yarn made of composite fibers so that the weft is

passed over the paired selvage yarns in a winding manner so
as to proceed; a device that continuously supplies a number
of warps of reinforcing fiber yarns onto the upper face and
lower face of the winding weft; a device that continuously
5   supplies warps of multifilament fusion-bonding yarns made
of composite fibers as second warps; a device which places
the warps in a manner so as to cover either the upper
portion or the lower portion of the warps of reinforcing
fiber yarns, and immediately after the resulting warps have
10   been subjected to a warping process, and supplied so that
the warps and the weft have been laminated, carries out
heating and pressurizing processes to fusion-bond the
fusion-bonding yarns used for the warps and weft, while the
multifilament fusion-bonding yarns made of composite fibers
15   of the warps and weft and the reinforcing fiber yarns of
the warps are fusion-bonded, and takes up the resulting
joined non-woven base fabric; and a manufacturing method by
which the manufacturing machine is operated.

(2) A reinforcing non-woven base fabric made from biaxial
20   reinforcing fibers.

(i) A reinforcing non-woven base fabric manufacturing
machine, which is constituted by at least: a device that
continuously supplies a pair of selvage yarns on both of
the right and left sides; a device that continuously
25   supplies a multifilament fusion-bonding yarn made from

composite fibers and a reinforcing fiber yarn alternately as wefts so that the wefts are passed over the paired selvage yarns in a winding manner so as to proceed; a device that continuously supplies a number of warps of

5   reinforcing fiber yarns onto the upper face and lower face of the winding wefts; a device that continuously supplies warps of multifilament fusion-bonding yarns made of composite fibers as second warps; a device which places the warps in a manner so as to cover either the upper portion

10   or the lower portion of the warps of reinforcing fiber yarns, and immediately after the resulting warps have been subjected to a warping process, and supplied so that the warps and the weft have been laminated, carries out heating and pressurizing processes to heat-bond the multifilament

15   fusion-bonding yarns of composite fibers used for the warps and weft with each other, while the multifilament fusion-bonding yarns made of composite fibers of the warps and weft and the reinforcing fiber yarns of the warps and weft are also fusion-bonded, and takes up the resulting joined

20   non-woven base fabric; and a manufacturing method by which the manufacturing machine is operated.

(ii) A reinforcing non-woven base fabric manufacturing machine, which is constituted by at least: a device that continuously supplies a pair of selvage yarns on both of

25   the right and left sides; a device that continuously

supplies a reinforcing fiber yarn as a weft so that the
weft is passed over the paired selvage yarns in a winding
manner so as to proceed; a device that continuously
supplies a number of warps of reinforcing fiber yarns onto

5   the upper face and lower face of the winding weft to carry
out warping and matching processes; a device that feeds a
mesh-shaped sheet formed by laminating a group of warp
yarns and a group of weft yarns that are arranged with
fixed intervals through multifilament fusion-bonding yarns

10   made of composite fibers; and a device which, immediately
after the warps and wefts have been laminated, inserts a
mesh-shaped sheet formed by multifilament fusion-bonding
yarns made of composite fibers from the upper portion or
the lower portion, or from both of the upper and lower

15   portions, to fuse the mesh-shaped sheet formed by
multifilament fusion-bonding yarns made of composite fibers,
by heating and pressurizing so that the wefts are bonded to
a non-woven base fabric through the heat bonding with the
warps, and takes up the resulting joined non-woven base

20   fabric; and a manufacturing method by which the
manufacturing machine is operated.

Example 1
     An olefin-based heat bonding multifilament (heat

25   bonding PYLEN (registered trademark) 680d; made by

Mitsubishi Rayon Co., Ltd.) was used as a support fibrous member. This support fibrous member, which is a multifilament having a core-sheath structure, has a core portion composed of polypropylene having a melting point of

5   165°C and a sheath portion composed of polyethylene having a melting point of 98°C, with 60 filaments having a thickness of 680 deniers, and the specific gravity thereof is 0.93.

A fusion-bonding mesh was manufactured by using a

10   heat-bonding mesh manufacturing machine as shown in Fig. 1 through the following processes.

The above-mentioned support fibrous member was used to form a mesh pattern in which a group of yarns 1 formed by arranging upper threads in the length direction with 2-cm

15   pitches and a group of yarns 2 formed by arranging lower threads with 2-cm pitches so that each thread is positioned between the upper threads 1 are placed, with a group of yarns 3 formed by arranging the same threads with 1-cm pitches in the width direction being sandwiched

20   therebetween.

This mesh material was fusion-bonded by using upper and lower electric heater rolls with the upper roll being set at 100°C and the lower roll being set at 80°C, under a nip pressure of 1.0 kg/cm at a line speed of 1 m/min, and

25   wound around a take-up roll 6; thus, a mesh was obtained.

The thickness of the resulting mesh was 0.1 mm at the thinnest portion and 0.12 mm at the thickest portion on each intersection, with a width of the thread being set to 1.2 mm.

5   Next, a reinforcing non-woven base fabric was manufactured by using a reinforcing non-woven base-fabric manufacturing machine shown in Fig. 2.

A carbon fiber yarn ("PYROFIL (registered trademark)" made by Mitsubishi Rayon Co., Ltd.) was used as a

10   reinforcing fiber in the length direction. The carbon fiber yarns of 12K, each having a yarn width of about 6 mm, were arranged in the length direction with 5-mm pitches to form a sheet without gaps; thus, a carbon-fiber yarn sheet 21 was prepared. The above-mentioned fusion-bonded mesh 24

15   was inserted from under this carbon fiber yarn sheet along the sheet face, and passed between electric heater rolls 22 and 23 placed in upper and lower positions in an S-letter shape, and then fusion-bonded under a nip pressure of 1.0 kg/cm at a roll temperature of 100°C at a line speed of 1

20   m/min; thus, a reinforcing non-woven base fabric of the present invention was obtained.

The cross section of the yarn in the width direction of the resulting reinforcing non-woven base fabric was observed under an electron microscope. Fig. 4 shows the

25   photographs. The sheath portions were fused into an

integral part, while each of the core portions was

maintained in its original shape. No voids such as bubbles

were observed between the support fibrous members. The

reinforcing non-woven base fabric was bonded to the carbon

5   fiber yarn sheet through an anchor effect by polyethylene

that forms the sheath portions having a low melting point.

The one-direction reinforced carbon fiber yarn sheet

was bound through the anchor effect by an olefin mesh that

had no water-absorbing property, and since the olefin mesh

10   was inherently thin and flexible, the resulting reinforcing

non-woven base fabric was flexible, and also allowed to

maintain its sheet shape. Moreover, since the olefin mesh,

used for the binding material, contained no bubbles, the

reinforcing non-woven base fabric was less susceptible to a

15   reduction in its strength, even when used for FRP or the

like.

Even when the thickness of the fibers (filaments) to

be used for the fusion-bonded mesh was made thinner to 340d

or 170d, there was no change in the binding effect; thus,

20   it is found that these fibers can be used for forming a

reinforcing non-woven base fabric.

Since olefin-based heat-bonding multifilament fibers

are used, the specific gravity thereof is smaller than

glass fibers. Therefore, even in the case of the same

25   fineness, the actual cross-sectional area of the yarn is

greater than that of the glass fibers.

The thickness of each of yarns formed into a net is shown below for comparison.

Glass mesh	0.6 mm
Fusion-bonded mesh (680d)	1.2 mm
Fusion-bonded mesh (340d)	1.0 mm
Fusion-bonded mesh (170d)	0.8 mm

Since the face made in contact with the reinforcing fiber yarns is allowed to exert the binding effect, the fusion-bonded mesh of 170d is sufficiently to be used so as to obtain the binding effect in the same level as the glass mesh.

The weight of each of meshes per 1 m^2 is shown below for comparison.

Glass mesh	16 g/m^2
Fusion-bonded mesh (680d)	15 g/m^2
Fusion-bonded mesh (340d)	7.5 g/m^2
Fusion-bonded mesh (170d)	3.8 g/m^2

Comparative Example 1

A glass mesh was manufactured by using a glass mesh manufacturing machine shown in Fig. 3 through the following processes.

Glass fiber yarns (thickness: 300 deniers, specific gravity: 2.54) were used as warps to form a mesh pattern in

which a group of yarns 31 formed by arranging upper threads
in the length direction with 1-cm pitches and a group of
yarns 32 formed by arranging lower threads with 1-cm
pitches are placed so that each lower thread is superposed
5   on each upper thread, with a group of yarns 33 formed by
arranging glass fiber yarns (thickness: 600 deniers,
specific gravity 2.54) with 1-cm pitches in the width
direction being sandwiched therebetween.

The resulting mesh material was impregnated with a
10   thermoplastic emulsion resin (ethylene-vinyl acetate
copolymer resin: solid component 30 %) put in a resin
vessel 36. Successively, the mesh material was passed
through rubber rolls 34 and 35 (diameter: 100 mm, width: 40
cm) placed in upper and lower positions so that the
15   excessive resin was squeezed, and dried by a drying roll at
130°C; thus, a mash formed of glass fiber yarns was
obtained.

The thickness of the resulting mesh was 0.12 mm at the
thinnest portion and 0.19 mm at the thickest portion on
20   each intersection, with a width of the thread being 0.6 mm.

Next, a reinforcing non-woven base fabric was
manufactured by using a reinforcing non-woven base-fabric
manufacturing machine shown in Fig. 5.

A carbon fiber yarn ("PYROFIL (registered trademark)"
25   made by Mitsubishi Rayon Co., Ltd.) was used as a

reinforcing fiber in the length direction. The carbon

fiber yarns of 12K, each having a yarn width of about 6 mm,

were arranged in the length direction with 5-mm pitches to

form a sheet without gaps; thus, a carbon-fiber yarn sheet

5   51 was prepared. The above-mentioned mesh 54 made of glass

fiber yarns was inserted from under this carbon fiber yarn

sheet along the sheet face, and passed between electric

heater rolls 52 and 53 placed in upper and lower positions

in an S-letter shape, and then fusion-bonded under a nip

10   pressure of 30 kg/40 cm at temperatures of upper and lower

rolls of 150°C at a line speed of 1 m/min; thus, a

reinforcing non-woven base fabric of the present invention

was obtained.

The cross section of the yarn in the width direction

15   of the resulting reinforcing non-woven base fabric was

observed under an electron microscope. Fig. 6 shows the

photographs. There were found that there were voids among

the threads forming the mesh and also that with respect to

the mesh and the carbon fiber yarn sheet, the thermoplastic

20   resin impregnated in the mesh was fused and bonded to the

carbon fibers.

The bonding agent impregnated in the glass fiber yarns

has a water-absorbing property, and the bonding agent is

used for binding. Since the yarns that form the glass mesh

25   are also impregnated with the bonding agent, and then dried,

they are converged into a round shape to allow the mesh

itself to have a sufficient thickness. Since the fibers

forming the mesh are made of glass, the resulting

reinforcing non-woven base fabric lacks in flexibility,

5   making it difficult for the mesh to follow curved faces,

when used for FRP or the like. Since there are voids in

the mesh itself to be used for binding, the strength of the

mesh is reduced when used for FRP or the like.

10   Example 2

Yarns prepared by opening a carbon fiber yarn

("PYROFIL (registered trademark)" made by Mitsubishi Rayon

Co., Ltd.) of 12K into a yarn width of about 20 mm were

used as reinforcing fibers. A group of upper layer yarns

15   in which these yarns were arranged with 4-cm pitches in the

length direction as upper threads and a group of lower

layer yarns in which the yarns were arranged with 4-cm

pitches in a manner so as to be accumulated with an offset

of a 1/2-pitch so that each lower thread was positioned

20   between the upper threads were formed.

An olefin-based heat bonding multifilament (heat

bonding PYLEN (registered trademark) 170d; made by

Mitsubishi Rayon Co., Ltd.) was used as a support fibrous

member. This support fibrous member, which was a

25   multifilament having a core-sheath structure, had a core

portion composed of polypropylene having a melting point of
165°C and a sheath portion composed of polyethylene having
a melting point of 98°C, with 60 filaments having a
thickness of 170 deniers, and the specific gravity thereof

5   was 0.93.

The above-mentioned carbon fiber yarns were used as
warp yarn groups forming two upper and lower layers, and
the support fibrous members of olefin-based heat bonding
multifilament having a core-sheath structure were used as

10   wefts.

The wefts, aligned in the width direction with 1-cm
pitches, were inserted between the upper and lower layers
of the warps, and positioned therein. Next, an electric
heater roll having a stainless outer layer was placed as an

15   upper roll, and an electric heater roll, which had the same
size with an outer layer made of heat-resistant silicon
rubber, was placed as a lower roll, and the binding process
was carried out by using the fusion-bonding wefts under
conditions of an upper roll temperature of 100°C, a lower

20   roll temperature of 80°C, a nip pressure of 1.0 kg/cm and a
line speed of 1 m/min; thus, a fiber reinforcing non-woven
base fabric with one-direction reinforced was obtained.

The cross section of the resulting reinforcing non-
woven base fabric was observed, and in the same manner as

25   the reinforcing non-woven base fabric obtained in example 1,

the sheath portions were fused into an integral part, while each of the core portions was maintained in its original shape. Voids such as bubbles were hardly observed between the support fibrous members. The carbon fiber yarn sheet

5   was bonded through an anchor effect by polyethylene that forms the sheath portions having a low melting point.

The one-direction reinforced carbon fiber yarn sheet was bound through the anchor effect by olefin-based multifilament threads that had no water-absorbing property,

10   and since the olefin-based multifilament threads were inherently flexible, the resulting reinforcing non-woven base fabric was flexible, and also allowed to maintain its sheet shape. Since the olefin-based multifilament threads themselves, used for the binding material, contain no

15   bubbles, the strength is nor deteriorated, even when used for FRP or the like.

Since the binding is made by using only the wefts, the weight of the reinforcing non-woven base fabric per 1 m^2 becomes very small. It is possible to make the amount of

20   use of the support fibrous member to be used for binding greatly smaller. For this reason, in the case of application to FRP, the components other than the reinforcing fiber yarns can be extremely reduced.

The weight per 1 m^2 of each of the reinforcing non-

25   woven base fabrics in which the respective binding methods

are applied to a material in which, as shown in example 2, fiber-extended carbon fiber yarns of 12K with a width of 20 mm are arranged at intervals of 20 mm as reinforced fiber yarns is shown below.

5 ・Reinforcing non-woven base fabric of example 2 (using only wefts)   42 g/m^2

・Application of glass mesh (using mesh)

57 g/m^2 (Comparative Example 1)

・Application of fusion-bonded mesh (680d) (using mesh)

10   56 g/m^2 (Example 1)

・Application of fusion-bonded mesh (340d) (using mesh)

48 g/m^2

・Application of fusion-bonded mesh (170d) (using mesh)

44 g/m^2